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Simbeor Application Note #2017\_03, August 2017 © 2017 Simberian Inc.

# Identification of dielectric and conductor roughness models with differential lines



Simbeor®: Accurate, Productive, Cost-Effective Electromagnetic Signal Integrity Software...

### Outline

Model identification with GMS-parameters

- Step 1: Measure S-parameters for 2 line segment and ensure quality and consistency
- Step2: Extract GMS-parameters
- Step 3: Create model of line segment and compute GMS-parameters
- Step 4: Identify dielectric and conductor roughness parameters
- Create model with two dielectrics (FEXT)
- Appendix: Results with causal Huray-Bracken roughness model



### Identification with GMS or SPP techniques



Y. Shlepnev, Broadband material model identification with GMS-parameters, EPEPS 2015.

Y. Shlepnev, Y. Choi, C. Cheng, Y. Damgaci, Drawbacks and Possible Improvements of Short Pulse Propagation Technique, EPEPS 2016.



### Step 1a: Measure S-parameters of 2 line segments, import into Simbeor and ensure quality

#### Quality of S-parameters of 24 inch in and 4 inch segment is good



See more on the import of S-parameters and quality assurance at <a href="http://kb.simberian.com/browse\_item.php?id=775">http://kb.simberian.com/browse\_item.php?id=775</a> <a href="http://kb.simberian.com/browse\_item.php?id=240">http://kb.simberian.com/browse\_item.php?id=240</a>

![](_page_3_Picture_4.jpeg)

## Step 1b: Ensure quality of test fixtures with TDR computed from S-parameters

#### TDRs of short and long segments are consistent, except the launch area Traces are about 46 Ohm

![](_page_4_Figure_2.jpeg)

See more on TDR computation at

http://kb.simberian.com/browse\_item.php?id=202

![](_page_4_Picture_5.jpeg)

### Step 2: Extract GMS-parameters

![](_page_5_Figure_1.jpeg)

See details and recommendations at <a href="http://kb.simberian.com/browse\_item.php?id=846">http://kb.simberian.com/browse\_item.php?id=846</a>

![](_page_5_Picture_3.jpeg)

## Step 2: Extract GMS-parameters – plot Magnitude and Phase Delay

![](_page_6_Figure_1.jpeg)

![](_page_6_Picture_2.jpeg)

## Step2: Extract GMS-parameters – use options to fix problems

![](_page_7_Figure_1.jpeg)

![](_page_7_Picture_2.jpeg)

## Step 3a: Compute GMS-parameters of line segment – cross section

![](_page_8_Figure_1.jpeg)

![](_page_8_Picture_2.jpeg)

## Step 3b: Compute GMS-parameters of line segment – model 20 inch diff strip segment

![](_page_9_Figure_1.jpeg)

![](_page_9_Picture_2.jpeg)

### Step 3c: Plot GMS-parameters of the model

![](_page_10_Figure_1.jpeg)

Elements GMS[1,3] – odd or differential mode transmission, GMS[2,4] – even or common mode transmission Mode M1 is odd, mode M2 is even

The first adjustment can be done without SiTune – from the Phase Delay we can see that the Dk and LT should be much lower (4.2 and 0.02@ 1 GHz are specified as the starting point)

![](_page_10_Picture_5.jpeg)

### Step 4a: Manually adjust Dk and LT to have model GMS-parameters closer to measured

#### For instance, adjust Dk to 3.7 and LT to 0.005 and re-run the analysis

![](_page_11_Figure_2.jpeg)

![](_page_11_Picture_3.jpeg)

### Step 4b: Manual adjustment of resistivity

![](_page_12_Figure_1.jpeg)

#### RR=1.25 gives better DC match, but this is questionable adjustment!

![](_page_12_Picture_3.jpeg)

## Step 4c: Bring model parameters into SiTune for the optimization

![](_page_13_Figure_1.jpeg)

![](_page_13_Picture_2.jpeg)

### Step 4c: Set up goal for Dk

#### c) From 1 to max b) Match Phase Delay to a) For GMS odd mode frequency (20 GHz Measured GMS-par. transmission parameter in this case) × Simulat Variable Value # Element Value Simulation/Polyline С Step GoalType А В Fmin, GHz Fmax, GHz We Operator Model. 5 1 S[1,3] Simulation Measured.diff.Simulation(1) 20. Model:Materials -> FR4 -> RelativePermittivity 3.7 PhaseDelay none none none 1. Add Row Model:Materials -> FR4 -> LossTangent 5.e-3 0 Model:Materials -> Copper -> RelativeResisti... 1.25 0 Model:Materials -> Copper -> SR1 0. [um] 0 Model:Materials -> Copper -> RF1 2. 0 $\langle \rangle$ < + Step: 5 Auto-S 3.7 % Min: 1.e-10 Max: Optimize d) Click "Optimize" button

Optionally, check "Same Thread Simulation" in Solution -> Configuration -> Optimizer, to run all simulations during the optimization in one thread (each simulation will be parallelized if necessary)

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Output Models	Solvers General			Rational Compactor		
RCM Passivity	Optimizer Mess		Messa	ge	Matrix	
Step Chang	ge Limit: [	1.002		[1., 1.5]		
Maximal Number of Steps:		5000		[1, 100000]		
Minimal Error: 0.0001				[0., 1000.]		
Cost Fi	unction:	1		[-4, 4]		
Step Change Algorithm:		2		[1, 2]		
Normalized Group Delay Scale:		10		[1., 1000000000.]		
Magnitude Scale:		10 [1.		[1., 1000	., 1000000000.]	
Number of Curves To Keep:		20	[0, 1000]		1	
Auto Freeze Lattice Box Before Optimization						
Same Thread Simulations and Optimization (as before version 2017)						
Tip: Change configuration only if optimizer hangs or recommended by support.						

![](_page_14_Picture_4.jpeg)

### Step 4c: Dk optimization result

#### Dk value matching measured and simulated GMS Phase delay

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1							

#### Final RMS Error

![](_page_15_Picture_4.jpeg)

### Step 4d: Set up goad for LT

![](_page_16_Figure_1.jpeg)

#### d) Run Optimization, Clean Curves

![](_page_16_Picture_3.jpeg)

## Step 4e: Identify conductor roughness model

![](_page_17_Figure_1.jpeg)

#### d) Run Optimization, Clean Curves

![](_page_17_Picture_3.jpeg)

### Step 4e: Analysis of preliminary results

![](_page_18_Figure_1.jpeg)

#### To improve accuracy, repeat step 4c

9/11/2017

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lectromagnetic Solution

### Results are acceptable, but not perfect

![](_page_19_Figure_1.jpeg)

Higher measured dispersion in Phase Delay indicates that LT should be larger (dispersion) The problem is with the matching RR at DC that resulted in larger value of resistance RR=1.25 – this is questionable result (resistance 25% of annealed copper)! Solution – set RR back to 1 (annealed copper) and redo the matching...

![](_page_19_Picture_3.jpeg)

### New results with RR=1

![](_page_20_Figure_1.jpeg)

![](_page_20_Picture_2.jpeg)

### What about the even mode?

![](_page_21_Figure_1.jpeg)

*Problem: Model contains only one dielectric* – cannot match simultaneously odd and even mode – though, it may be acceptable if FEXT is not large Solution: Create model with the additional layer of dielectric around the strips – see next slides...

![](_page_21_Picture_3.jpeg)

### Model with inhomogeneous dielectric

![](_page_22_Picture_1.jpeg)

### Predominantly resin

	85-L3-4inch	85-L3-24inch	
Parameter	Avg.	Avg.	
а	5.66	5.67	
b	7.41	7.35	
с	6.51	6.58	
d	6.67	6.74	
е	0.65	0.65	
f	5.80	5.82	
g	5.15	5.16	

![](_page_22_Figure_4.jpeg)

![](_page_22_Picture_5.jpeg)

## Simultaneously match odd and even mode GMS-parameters

a) Use parameters identified for homogeneous dielectric as the starting point

b) Bring relative permittivities of the base material (FR4) and fill c) Alternatively set goals for Phase delays for 2 modes and optimize

![](_page_23_Figure_3.jpeg)

Final dielectric models: Wideband Debye FR4 Dk=3.54, LT=0.0058 @ 1 GHz; Resin Dk=3.76, LT=0.0058 @ 1 GHz; Copper roughness model: Groiss SR=0.19 um, RF=2.75

![](_page_23_Picture_5.jpeg)

## Compare raw single-ended S-parameters for 24 inch segment

24-inch segment model with ideal 100 Ohm connector model

![](_page_24_Figure_2.jpeg)

![](_page_24_Picture_3.jpeg)

## Compare raw differential S-parameters for 24 inch segment

24-inch segment model with ideal 100 Ohm connector model

![](_page_25_Figure_2.jpeg)

### Compare TDR for 24 inch segment

![](_page_26_Figure_1.jpeg)

Requires further investigation - see appendix...

![](_page_26_Picture_3.jpeg)

### Conclusion

- Always identify or validate dielectric, conductor and conductor roughness models
- Use of GMS-parameters is simplest and most accurate technique for the material model identification
- Differential strip is useful to identify dielectric inhomogeneity and fit 2 dielectric models simultaneously
- Use homogeneous dielectric if no FEXT observed or FEXT is not a part of design
- Use two dielectric models to match phase delay of two modes – it leads to match in the FEXT

![](_page_27_Picture_6.jpeg)

## Appendix: Causal Huray-Bracken roughness model

$$K_{sr} = 1 + \sum_{k} \left( \left( RF_{k} - 1 \right) \cdot \left( 1 + \left( 1 - i \right) \frac{\delta_{s}}{2r_{i}} \right)^{-1} \right) \quad \delta_{s} = \sqrt{\frac{1}{\pi \cdot f \cdot \mu \cdot \sigma}} \qquad Z_{rough} = K_{sr} \cdot (1 + i) \cdot \delta_{s}$$

*RFi* - roughness factor, defines maximal growth of losses due to all balls with radius ri; ri – ball radius (SRi parameter in Simbeor);

![](_page_28_Figure_3.jpeg)

J. E. Bracken, A Causal Huray Model for Surface Roughness, DesignCon 2012

![](_page_28_Picture_5.jpeg)

### Appendix: Results with causal Huray-Bracken model

- a) Use parameters identified for inhomogeneous dielectric as the starting point, set LT to 0.002 (specs);
- b) Optimize roughness model parameters (SR1, RF1), to match GMS IL from 2 to 20 GHz
- c) Adjust Dk of FR4 and Resin, to match the even and odd mode Phase Delay

![](_page_29_Figure_4.jpeg)

Final dielectric models: Wideband Debye FR4 Dk=3.465, LT=0.002 @ 1 GHz; Resin Dk=3.63, LT=0.002 @ 1 GHz; Copper roughness model (RR=1): Huray-Bracken SR=0.2 um, RF=8.134 If copper relative resistance is adjusted to RR=1.2, Huray-Bracken model is SR=0.2, RF=7.75

![](_page_29_Picture_6.jpeg)

#### Appendix: Validation with causal Huray-Bracken model

24-inch segment model with ideal 100 Ohm connector model

![](_page_30_Figure_2.jpeg)

![](_page_30_Picture_3.jpeg)

### Appendix: Validation with causal Huray-Bracken model

24-inch segment model with ideal 100 Ohm connector model

![](_page_31_Figure_2.jpeg)

![](_page_31_Picture_3.jpeg)

### Appendix: TDR for 24 inch segment with Huray-Bracken roughness model

![](_page_32_Figure_1.jpeg)

![](_page_32_Picture_2.jpeg)

### Appendix: TDR for 24 inch segment with Huray-Bracken roughness model

![](_page_33_Figure_1.jpeg)

TDR can be used to validate the relative resistivity in addition to matching GMS IL at the lowest frequency...

![](_page_33_Picture_3.jpeg)

### Simberian Inc.

- Mission
  - Build accurate, easy-to-use, and cost-effective electromagnetic software for high-speed electronic design automation
- □ Incorporated in USA on February 28, 2006
  - Founder and President Yuriy Shlepnev
    - PhD in in computational electromagnetics
    - 25-years experience in building electromagnetic software
- Development in Westlake Village, USA, St. Petersburg and Voronezh Russia

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- Web: <u>www.simberian.com</u>
- Support knowledge base <u>www.kb.simberian.com</u>

![](_page_34_Picture_12.jpeg)